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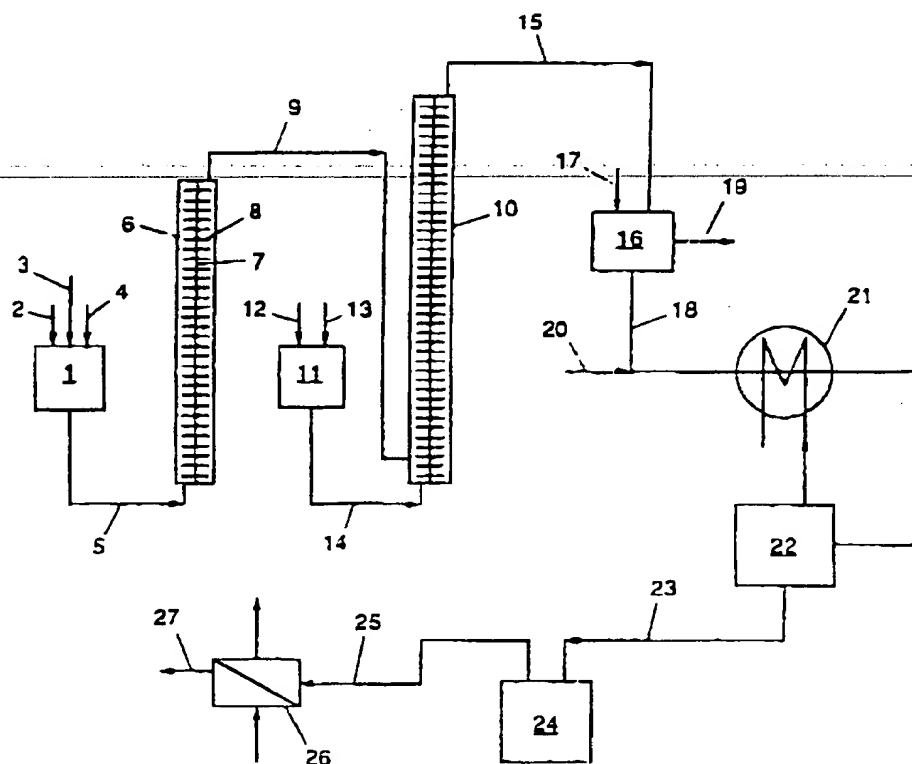
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## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

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<b>(21) International Application Number:</b> PCT/NL92/00006  <b>(22) International Filing Date:</b> 10 January 1992 (10.01.92)  <b>(30) Priority data:</b> 9100050                      11 January 1991 (11.01.91)      NL  <b>(71) Applicant (for all designated States except US):</b> HEINEKEN TECHNISCH BEHEER B.V. [NL/NL]; 2e Wetering- plantsoen 21, NL-1017 ZD Amsterdam (NL).  <b>(72) Inventor: and</b> <b>(75) Inventor/Applicant (for US only):</b> VERSTEEGH, Christia- an, Willem [NL/NL]; Noordeinde 128, NL-2611 WV Delft (NL).  <b>(74) Agent:</b> SMULDERS, Th., A., H., J.; Vereenigde Octrooib- bureaux, Nieuwe Parklaan 97, NL-2587 BN The Hague (DE).		<b>(81) Designated States:</b> AT, AT (European patent), AU, BB, BE (European patent), BF (OAPI patent), BG, BJ (OAPI patent), BR, CA, CF (OAPI patent), CG (OAPI patent), CH, CH (European patent), CI (OAPI patent), CM (OAPI patent), CS, DE, DE (European patent), DK, DK (European patent), ES, ES (European patent), FI, FR (European patent), GA (OAPI patent), GB, GB (Eu- ropean patent), GN (OAPI patent), GR (European pa- tent), HU, IT (European patent), JP, KP, KR, LK, LU, LU (European patent), MC (European patent), MG, ML (OAPI patent), MN, MR (OAPI patent), MW, NL, NL (European patent), NO, PL, RO, RU, SD, SE, SE (Eu- ropean patent), SN (OAPI patent), TD (OAPI patent), TG (OAPI patent), US.  <b>Published</b> <i>With international search report.</i> <i>In English translation (filed in Dutch).</i>

**(54) Title:** A PROCESS FOR THE CONTINUOUS PREPARATION OF WORT**(57) Abstract**

This invention relates to a process for the continuous preparation of wort, comprising the continuous enzymatic conversion of malt in at least one rotating disc contactor and separation of spent grain from mash in a separation unit, as well as a process for the continuous preparation of wort, comprising the continuous gelatinization and enzymatic liquefaction of a mixture based on unmalted grain, malt and/or an enzyme source and water in a rotating disc contactor, addition of malt and/or enzyme source to the product obtained, enzymatic conversion of the product obtained and separation of the spent grain from the mash in a separation unit.



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Title: A process for the continuous preparation of wort

This invention relates to a process for the continuous preparation of wort, comprising the continuous enzymatic conversion of malt to a mash. Moreover, the invention is concerned with the continuous gelatinization and enzymatic liquefaction of a mixture based on unmalted grain, an enzyme source and water. The invention also relates to a continuous process for the preparation of wort, comprising the above steps followed by a continuous separation of the spent grain from the mash.

When making beverages from cereals, more in particular when brewing beer, wort is used. A conventional preparation of wort occurs by mixing the starting materials, e.g., comprising unmalted grain (maize) and water. The solid materials are first crushed (pulverized) and then mixed with the water. The resulting suspension is kept for some time at a temperature of at least 40°C in the presence of an enzyme source, e.g., malt. Gelatinization and liquefaction thereby occur. In a next step the enzymatic conversion of the mixture (mash) is continued after supplementary addition of malt and/or an external enzyme source.

It is also possible to prepare wort on the basis of malt and water. Then the first step is omitted.

The product thus obtained consists mainly of water, insoluble components of the raw materials, as well as soluble components thereof, such as fermentable and unfermentable sugars and proteins. In the conventional method this mixture is filtered to remove the insoluble components, the spent grain. The filtrate or extract is the wort. For brewing beer, hop is then added to the wort, which is boiled. The flakes formed, if any, are removed, and the wort is cooled to about 8°C and fermented.

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In the past much research was done into the continuous performance of the steps of gelatinization, liquefaction and conversion to fermentable and unfermentable sugars. In particular, research was done into the performance of these steps in an envelope heat exchanger (Food Engineering Int'l, Dec. 76, pp. 22-27). This research, however, did not result in a commercial use.

The object of this invention is to provide a method for the continuous preparation of wort, in which no problems occur with respect to contamination and the like, and which has the additional advantage that there are no or substantially no restrictions relative to the particle size of the raw materials to be used.

The invention therefore relates to a process for the continuous preparation of wort, comprising the continuous enzymatic conversion of malt in a rotating disc contactor and separation of spent grain from mash in a separation unit. The invention also relates to such a process comprising the continuous gelatinization and enzymatic liquefaction of a mixture based on unmalted grain, an enzyme source and water in a rotating disc contactor, addition of malt and/or an enzyme source to the resulting product, enzymatic conversion of that product and separation of the spent grain from the mash in a separation unit.

Preferably, the enzymatic conversion is carried out continuously in a rotating disc contactor.

It is possible to carry out the process in one or more rotating disc contactors. The number of contactors partly depends on the nature of the raw materials to be used.

When unmalted grain is used, two reaction steps are carried out, in the first of which the pulverized material is gelatinized and liquefied under the influence of an enzyme system. This enzyme system often originates from malt. In a second step malt and/or an additional enzyme system is added, and further reaction occurs. It is thus necessary to carry out two reaction steps, which may be done advantageously in two reactors, although it is also possible to use one reactor, on

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condition that it is provided with inlets in the proper places. When only malt is used, without unmalted grain, it is sufficient to carry out only the second reaction step, which may be done in one reactor.

5 Surprisingly, it has been found that it is excellently possible with the process according to the invention to prepare wort without the occurrence of the problems that are inherent to the known continuous wort preparation methods.

10 The solid components, such as malt and unmalted grain, used according to the invention are first pulverized, e.g., in a hammer mill, to a particle size which can pass through screens with a mesh size of from (5  $\mu\text{m}$ ) to 5 mm.

The pulverized solid materials are mixed with the water and fed to the reactor or reactors. When unmalted grain  
15 is used, a temperature ranging from 40 to 100°C is maintained in a first reaction step. Gelatinization and liquefaction under the influence of the enzyme system present thereby occur. In the second reaction step malt and/or the enzyme source and water are added, together with the product obtained  
20 in the first reaction step. In this reaction step enzymatic conversion occurs. The temperature in this reaction step generally ranges from 30 to 80°C. When no unmalted grain is used, this is the only reaction step, and a mixture of malt and water is fed to this reaction step.

25 According to the invention a rotating disc contactor is used, which is a known type of column reactor as described in, e.g., Kirk-Othmer, Encyclopedia of Chemical Technology, Third Edition, Vol. 9, page 702.

Such a reactor generally consists of a column provided  
30 with a central agitator shaft having attached thereto 10 or more discs or plates. These discs or plates cover at least 80% of the cross section of the column. In general, this surface does not exceed 95%. By rotating the shaft and the discs in the column a proper dispersion of the solid matter in the  
35 liquid takes place.

In connection with the desired possibility to clean the column a system is preferably used in which the shaft can

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be easily removed, e.g., due to the absence of baffles in the column.

The use of a rotating disc contactor has the surprising advantage that the particle size of the raw materials can be adjusted almost independently of the apparatus used. In combination with the use of a continuous wort filtration this means that the particle size of the starting materials can be chosen almost freely, so that this particle size can be adjusted optimally, independently of the nature of the process apparatus.

The separation of the spent grain from the mash can be carried out in different ways. It is possible, e.g., to carry out a conventional wort filtration. This is in particular a possibility in the situation that an existing brewhouse is to be extended. By simply adding a rotating disc contactor in combination with a buffer vessel the capacity and effectiveness of a brewhouse can be considerably increased. In that case the enzymatic conversion preferably also occurs in a conventional noncontinuous manner.

The advantages of the process according to the invention can be better utilized, however, if the wort filtration is also carried out continuously, e.g., using a combination of mixers and settling units. Preferred is the use of a membrane filtration, since this results in an optimum effect in the continuity of the process and the efficiency of the wort preparation.

A preferred embodiment of the process according to the invention is characterized in that the spent grain is separated from the mash in at least one membrane filtration unit, if desired followed by addition of hop to the wort and boiling of the wort.

The membrane filtration is effected by using at least one membrane filter, but preferably by using a multi-stage filter, e.g., a multi-stage counterflow filtering apparatus, such as a three-stage apparatus or a multi-stage cross-flow filtering apparatus.

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The membranes in the membrane filter have a pore size not exceeding 2.0  $\mu\text{m}$ , preferably ranging from 0.1 to 1.5  $\mu\text{m}$ . Such a pore size results in an optimum activity of the filtration unit, because at this pore size a good clear wort is obtained with a high extract yield. The membrane filter also has a good self-cleaning effect. The material of the membrane is not very critical. Of special importance is the mechanical stability at the temperature of the wort to be filtered. In addition, the material must be suitable for use in contact with foods.

Particularly suitable are membranes on the basis of ceramic materials.

It is to be noted that European patent application 0 265 152 discloses the filtration of wort using a membrane having a pore diameter of from 10.0 to 100.0  $\mu\text{m}$ . As appears from the text of that publication, the membrane is intended to separate the spent grain from the mash, the advantage residing in that a smaller particle size of the starting products can thus be used. This has advantages relative to the extraction efficiency of the sugars from the raw materials.

However, the membrane filtration according to this publication does not result in a clear wort which is simply adapted for further use. In particular, it appears from the text of the application that the wort as initially produced is not free from suspended particles, so that a supplementary filtration is required. This is a drawback of this method.

When using a membrane having a pore size within the limits according to the present invention the extract yield is better than when using a membrane having larger pores. Moreover, less fouling of the membrane occurs. The latter has the advantage that the process can be carried out continuously, since much less cleaning of the membranes is required.

The wort obtained with the process according to the invention has a clarity measured as EBC units at 65°C of from 0.25 to 5. The clear wort is mixed with hop, and the mixture is boiled. Flocculation of material, such as proteins and polyphenols, may then occur. If desired, this flocculated

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material may be removed, e.g., in a separator. After cooling the wort to a temperature ranging from 2 to 25°C, preferably to about 8°C, the wort can be fermented to beer.

The boiling of the wort preferably occurs continuously, with recovery of at least part of the heat. Apparatuses suitable therefor are known from the literature. These apparatuses may be based, e.g., on multi-effect evaporators with a heat exchange of the spent gases with the liquid to be boiled. The heat can be advantageously used in the gelatinization, liquefaction and/or enzymatic conversion.

The cooled wort can be fermented, optionally after residence in a buffer vessel. The invention therefore also relates to a process for brewing beer using wort prepared as described above.

A surprising aspect of the process according to the invention resides in the fact that the particle size of the solid materials only slightly effects the activity of the filters, contrary to what is suggested in the cited European patent application.

The invention will now be illustrated with reference to the accompanying drawings, which shows an example of a process scheme according to a preferred embodiment of the invention, as well as an embodiment of two membrane filtration systems.

In the drawings, Fig. 1 shows a process scheme of a preferred embodiment of the process according to the invention. Fig. 2 shows a detailed embodiment of the three-stage counterflow membrane filtration. Fig. 3 shows an embodiment of a cross-flow membrane filtration.

The process scheme of Fig. 1 shows a mixer 1, to which water having a temperature of about 55°C, pulverized unmalted grain and pulverized malt are passed through lines 2, 3 and 4, respectively. After mixing, the mixture is passed through line 5 to the first rotating disc contactor 6, which comprises an agitator shaft 7 provided with discs 8. The reactor 6 is provided with heating elements, not shown, with which the

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reactor contents can be adjusted to and maintained at the desired temperature.

The product from the reactor 6 is passed through line 9 to the rotating disc contactor 10. Water of about 55°C and pulverized malt are passed through lines 12 and 13 to a mixer 11. The resulting mixture is passed through line 14 to the bottom of the column 10 where it is mixed after some residence time with the product from the reactor 6. Through a line 15 the resulting mash is passed to a membrane filtration 16, to which, in addition, water is passed through a line 17. Through a line 18 the resulting clear wort obtained is discharged from the membrane filtration unit. The spent grain is discharged through a line 19.

The clear wort is mixed with hop supplied through a line 20. The mixture of wort and hop is fed to a heat exchanger 21, in which it is preheated with heat from the boiling step. The preheated wort is fed to the wort boiler 22, in which it is boiled for some time. The boiled product is passed through a line 23 to the separator 24, in which flocculated materials, such as proteins and polyphenols, are separated. The clear boiled wort then passes through a line 25 into a cooler 26, in which it is cooled. Through a line 27 the wort can be discharged, e.g., to a fermentation.

Fig. 2 shows a possible arrangement of a three-stage counterflow membrane filtration.

In this Figure, the mash is passed through a line 51 to the first membrane filter 52, from which the clear wort is discharged through a line 53. Part of the retentate of the filter 52 is returned through a line 54 to the feed end of the filter, together with the permeate of the second membrane filter 55. The rest of the retentate is passed through a line 56 to the second membrane filter 55. The permeate of this membrane is returned through a line 57 to the first membrane filter. The retentate of the second filter 55 is partly returned to the feed end of the second membrane filter 55, through a line 58, while the rest is passed through a line 59 to the third membrane filter 60. The permeate of this third

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membrane filter 60 is returned through a line 61 to the feed end of the second membrane filter 55. Part of the retentate of the third filter 60 is returned through a line 62 to the feed end of the third filter 60, together with water passed through a line 63. The rest of the retentate, the spent grain, is discharged through a line 64.

The description of this system is based on a three-stage filtration unit, but it is of course possible to adapt the number of stages as required, using the same principle.

Fig. 3 shows an embodiment of a cross-flow filtration unit, on the basis of a three-stage equipment, but the number of stages can be adapted as required, using the same principle.

In Fig. 3, the mash is passed through a line 100 to the first membrane filter 101, from which the clear wort is discharged through a line 102. The retentate of the filter 101 is partly passed through a line 103 to the second membrane filter 104 and partly returned through a line 112 to the feed end of the filter 101. Through a line 105 water is passed to the feed end of the filter 104. The permeate of the membrane filter 104 is discharged through a line 106 and combined with the permeate of the first membrane filter 101. The retentate of the second filter 104 is partly passed through a line 107 to the third membrane filter 108, together with water supplied through a line 109, and partly returned through a line 113 to the feed end of the filter 104. The permeate of this third membrane filter 108 is combined through a line 110 with the permeate of the first two filters. The rest of the retentate, the spent grain, is partly discharged through a line 111 and partly returned through a line 114 to the feed end of the filter 108.

The invention will be further illustrated by an Example, but is not limited thereto.

#### EXAMPLE

To the mixer 1 of an apparatus, as shown in Fig. 1, are added per hour 5 kg maize, 2.5 kg malt and 22.5 l water

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having a temperature of 55°C. The maize and the malt were pulverized in a hammer mill to a particle size that can pass through a 1.5 mm screen. The mixture had a temperature of 50°C. The mixture was passed to a rotating disc contactor, in which the temperature was increased to 95°C. The total residence time of the mixture at 50°C was 5 min., while the residence time at 95°C was 10 to 15 min.

To the mixture 11 were added per hour 15 kg malt of the same particle size and 45 l water having a temperature of 55°C. The mixture obtained therein had a temperature of 50°C and was passed to the bottom of the second rotating disc contactor.

The product from the first rotating disc contactor was passed to the second rotating disc contactor at such a level that the residence time of the malt/water mixture was about 15 min. at 50°C. By admixing the hot product the temperature increased to 65°C. This temperature was maintained for 30 min., after which it was raised to 76°C, which temperature was maintained for another 5 min.

After this treatment a mash was obtained having an extract content of about 21.5%, which was passed to the membrane filtration unit 16. This unit was as shown in Fig. 2. The membrane filtration using membranes having a pore size of 0.4  $\mu\text{m}$  gave a wort having a clarity of 0.3 EBC units (at 65°C). After mixing with hop, boiling, separating flakes formed and cooling, a cold wort having a temperature of 8°C was obtained, which could be fermented to beer.

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CLAIMS

1. A process for the continuous preparation of wort, comprising the continuous enzymatic conversion of malt in at least one rotating disc contactor and separation of spent grain from mash in a separation unit.
- 5 2. A process for the continuous preparation of wort, comprising the continuous gelatinization and enzymatic liquefaction of a mixture based on unmalted grain, malt and/or an enzyme source and water in a rotating disc contactor, addition of malt and/or enzyme source to the product obtained,  
10 enzymatic conversion of the product obtained and separation of the spent grain from the mash in a separation unit.
3. A process as claimed in claim 2, wherein the enzymatic conversion is carried out continuously in a rotating disc contactor.
- 15 4. A process as claimed in claims 1-3, wherein the solid materials to be used can pass through screens with a mesh size of from 5  $\mu\text{m}$  to 5 mm.
5. A process as claimed in claims 1-4, wherein the  
20 separation of the spent grain from the mash is carried out in a membrane filtration unit having a pore size of the filter not exceeding 2.0  $\mu\text{m}$ , or in a conventional filter, or in a mixing/settling unit, resulting in a clear wort.
6. A process as claimed in claim 5, wherein the  
25 separation of the spent grain from the mash is carried out continuously in a membrane filtration unit.
7. A process as claimed in claim 5 or 6, wherein the membrane filtration unit comprises at least three stages.
8. A process as claimed in claims 1-7, wherein the wort is boiled after addition of hop.

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9. A process as claimed in claim 8, wherein the wort is boiled in a system with recovery of heat.

10. A process as claimed in claim 9, wherein the heat is used in the gelatinization, liquefaction and/or enzymatic conversion.

11. A process as claimed in claims 1-10, wherein the boiled wort, optionally after clarification, is cooled and fermented.

12. A process for brewing beer, comprising the fermentation of wort obtained using the process as claimed in claims 1-11.

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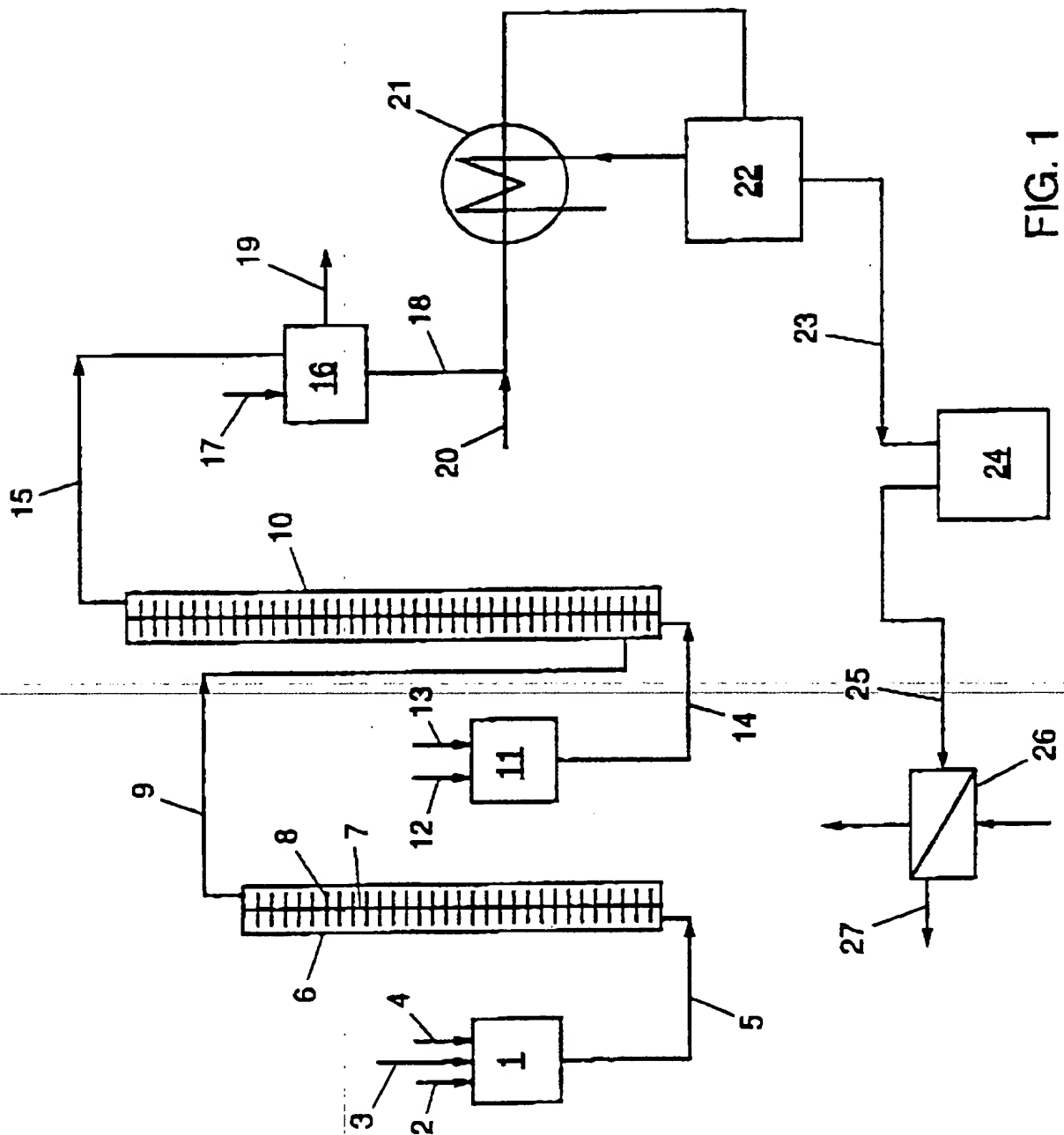


FIG. 1

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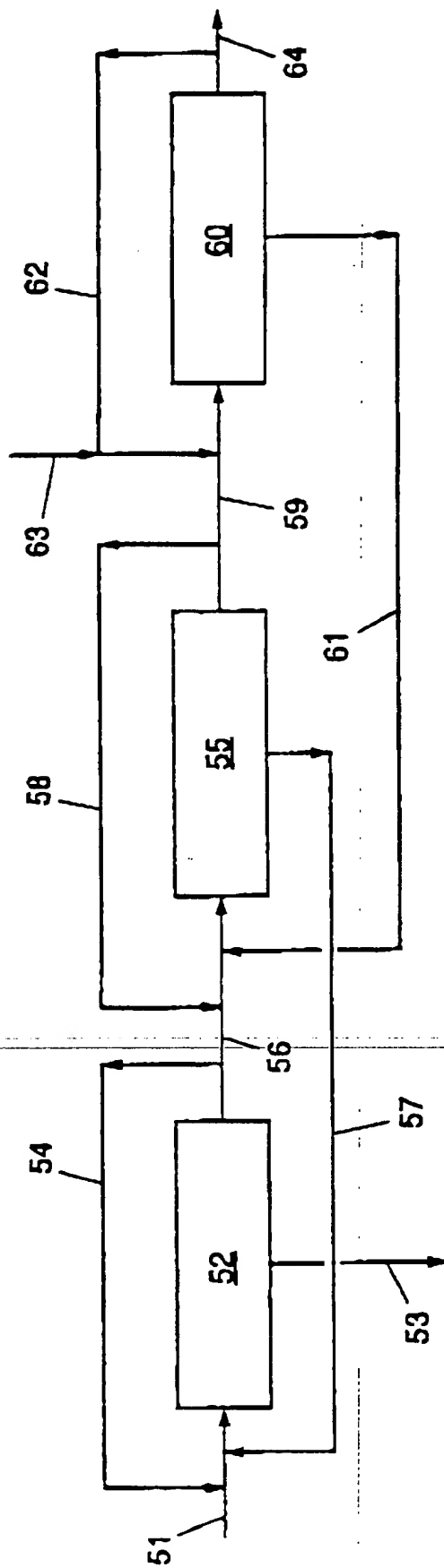


FIG. 2

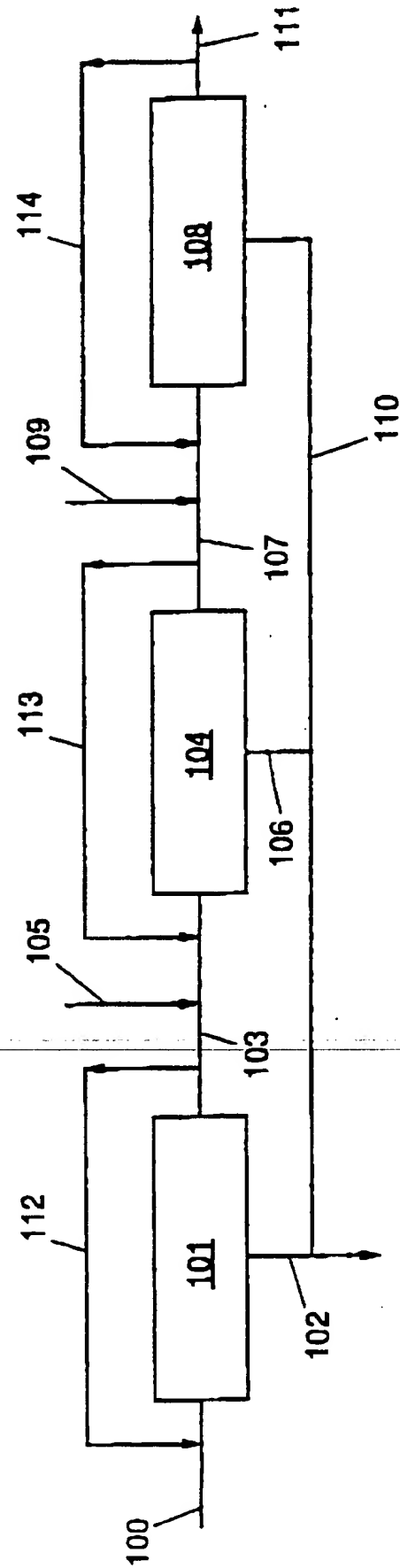


FIG. 3



## INTERNATIONAL SEARCH REPORT

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International Application No.

I. CLASSIFICATION OF SUBJECT MATTER (If several classification symbols apply, indicate all)<sup>6</sup>

According to International Patent Classification (IPC) or to both National Classification and IPC

Int.Cl. 5 C12C7/16;

C12C7/06

## II. FIELDS SEARCHED

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Documentation Searched other than Minimum Documentation  
to the Extent that such Documents are Included in the Fields Searched<sup>8</sup>III. DOCUMENTS CONSIDERED TO BE RELEVANT<sup>9</sup>

Category <sup>10</sup>	Citation of Document <sup>11</sup> with indication, where appropriate, of the relevant passages <sup>12</sup>	Relevant to Claim No. <sup>13</sup>
X Y A	US,A,3 216 345 (F. L. LLOYD) 9 November 1965  see claims; figures ---	1-3,12 1,4-6 8,11
A  Y A Y	DE,B,1 222 454 (ARTHUR GUINNESS SON AND COMPANY) 11 August 1966 see claims; figures  ---	1-3,12  1,4-6 8,11
Y	EP,A,0 265 152 (THE BREWING RESEARCH FOUNDATION) 27 April 1988 cited in the application see column 1, line 55 - column 2, line 47; claims; figures ---	1,4,6
A	US,A,2 309 989 (B.E.SALTZMAN) 2 July 1941 see claims; figures ---	8-10
	-/-	

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## IV. CERTIFICATION

Date of the Actual Completion of the International Search

09 MARCH 1992

Date of Mailing of this International Search Report

25. 03. 92

International Searching Authority

EUROPEAN PATENT OFFICE

Signature of Authorized Officer

COUCKE A.O.M. 

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III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)		Relevant to Claim No.
Category *	Character of Document, with indication, where appropriate, of the relevant passages	
A	US,A,3 048 489 (P. BLUM) 7 August 1962 see the whole document	1,8, 10-12
A	BRAUWELT INTERNATIONAL, NO.2, 1984. DE ANON. OF WORT AND BEER * whole document *	1,4,5
A	US,A,2 127 759 (J.F. SILHAVY) 23 August 1938	

# ANNEX TO THE INTERNATIONAL SEARCH REPORT ON INTERNATIONAL PATENT APPLICATION NO.

 NL 9200006  
SA 55853

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file as of the date of the search. The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information. 09/03/92

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US-A-3216345		None	
DE-B-1222454		None	
EP-A-0265152	27-04-88	AU-B- 599707	26-07-90
		AU-A- 7957387	21-04-88
		JP-A- 63185365	30-07-88
		US-A- 4844932	04-07-89
US-A-2309989		None	
US-A-3048489		None	
US-A-2127759		None	